

All Vibration is a Summation of Mode Shapes

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Topics of this Presentation

- **Fundamental Law of Modal Analysis (FLMA)**: All vibration is a *summation of mode shapes*
- *FEA mode shapes* will be used to “*decompose*” and then “*expand*” experimental data to include DOFs that were not experimentally acquired
- *Only FEA mode shapes* will be used, not their frequency or damping
- Mode shapes from an *FEA model* with *free-free boundary conditions* and *no damping* will be used

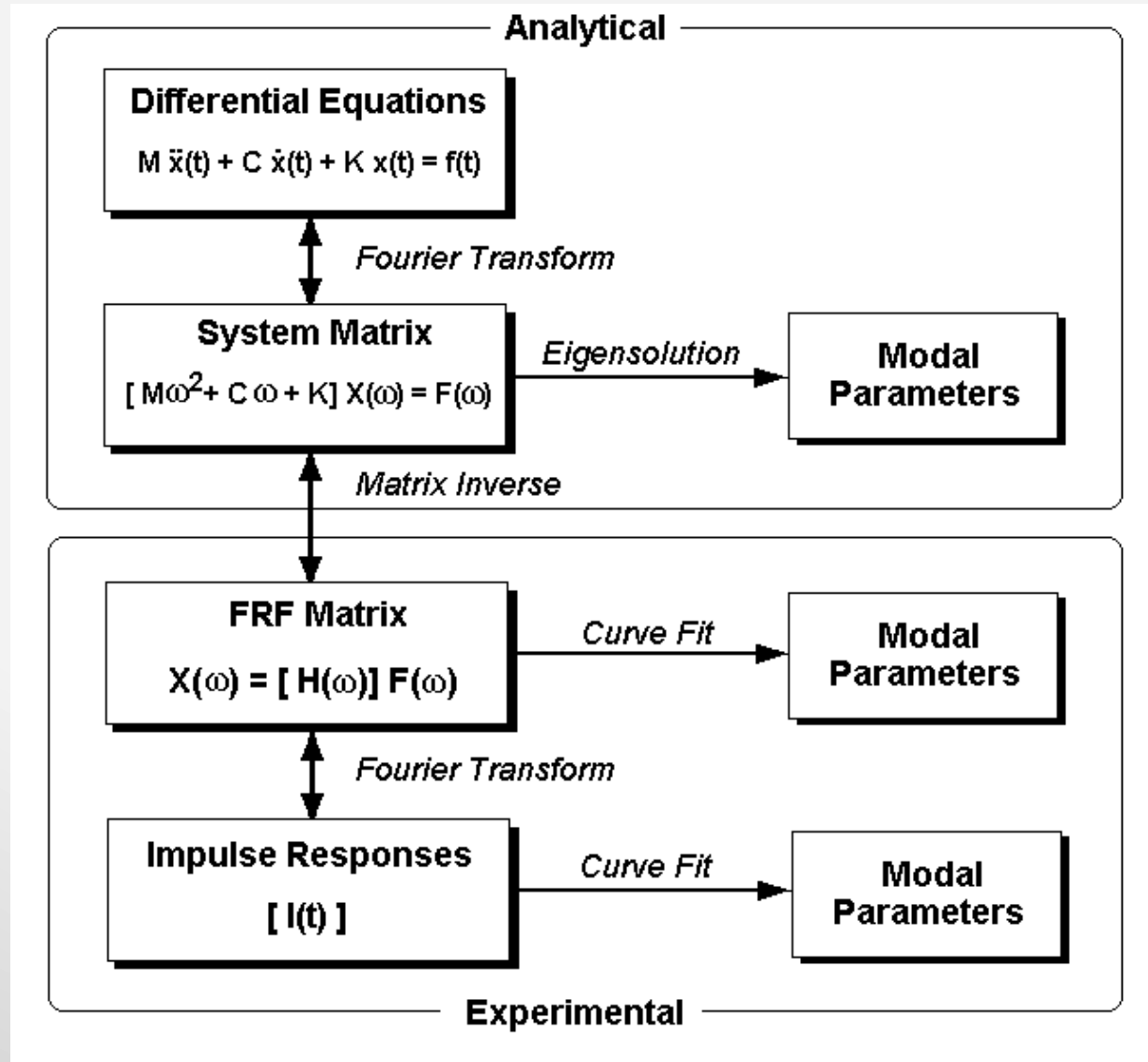
What is a Mode of Vibration?

- A mode of vibration is a **mathematical representation** of a **structural resonance**
- Any structure made out of **elastic materials** will **exhibit resonant vibration**
- When **dynamic forces are applied** and **energy is trapped** within the boundaries of a structure, **it will resonate**
- When energy is trapped within the material boundaries of a structure, it causes a **“standing wave deformation”**. This is called a **mode shape**
- Some modes will **readily absorb energy** causing a structure to resonate
- A structure in resonant vibration can be thought of as a **mechanical amplifier**. A **small dynamic load** can cause **excessive deformation**

Two Ways to Create Mode Shapes

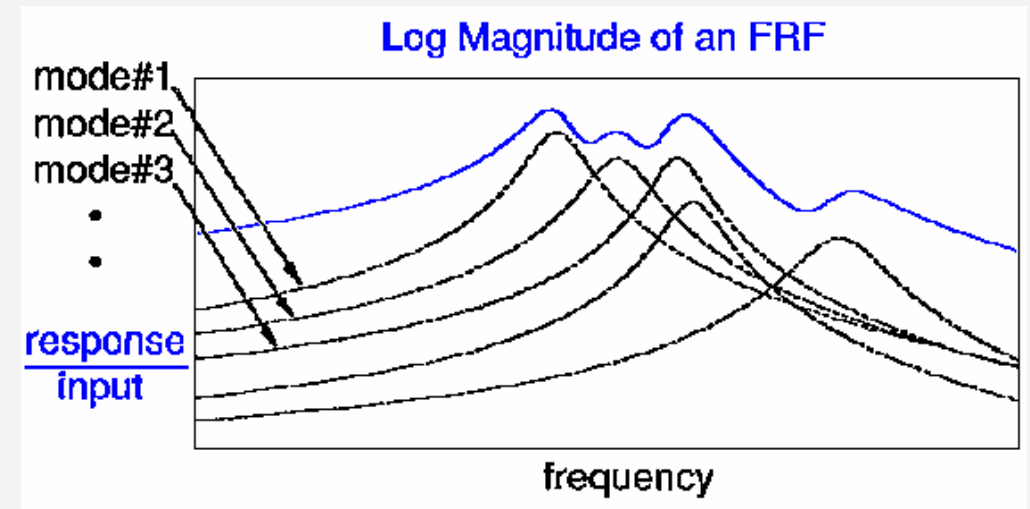
- **Experimental Modal Analysis (EMA):** EMA mode shapes are obtained by *curve fitting* a set of experimentally derived time waveforms or frequency spectra that characterize the structural dynamics
- **Finite Element Analysis (FEA):** FEA mode shapes are obtained as the *eigensolution* of a set of differential equations that characterize the structural dynamics
- **Both EMA & FEA** are *based upon FLMA*

Two Ways to Create Mode Shapes



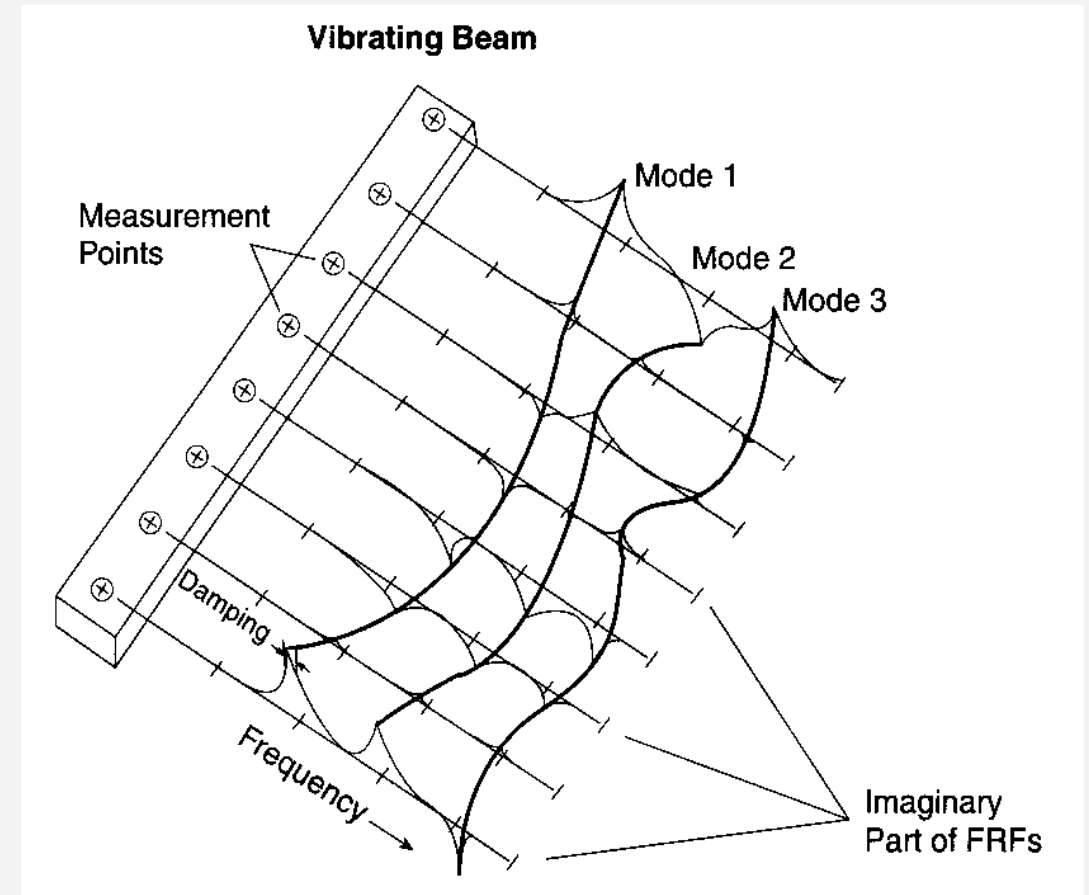
Modal Testing

- All **dynamic response data** is acquired as a **time waveform**
- **Without loss of information**, the **FFT** transforms each time waveform into its corresponding **Fourier spectrum**
- An **Auto spectrum, Cross spectrum, FRF, ODS FRF**, or **Transmissibility** is calculated from a Fourier spectrum
- **All modal testing** is **based on FLMA**
- **All vibration data** is a **summation of resonance curves**, each curve due to **a mode of vibration**



Curve Fitting

- **Multiple time waveforms or frequency spectra** are needed to **define EMA mode shapes**
- **Each mode** is defined with **three parameters**
 - **Modal frequency**
(the **frequency** of a resonance peak)
 - **Modal damping**
(the **width** of a resonance peak)
 - **Mode shape**
(the **magnitude & phase** of each resonance peak at the **same frequency**)



Expanding Experimental Data

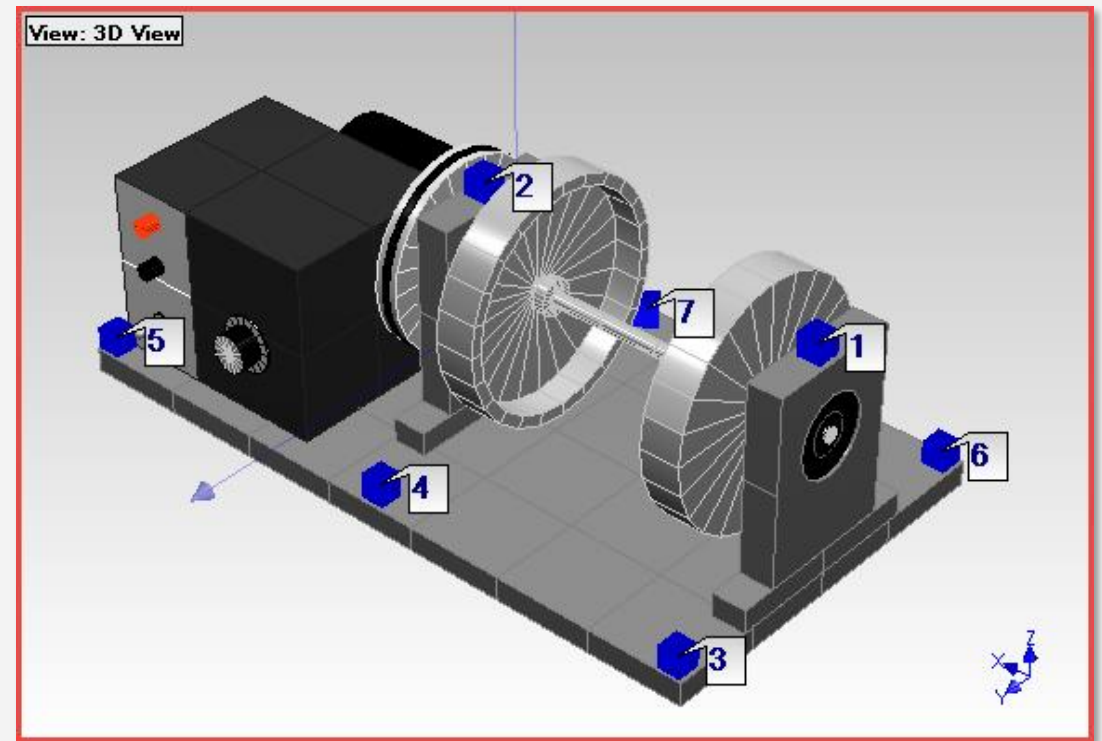
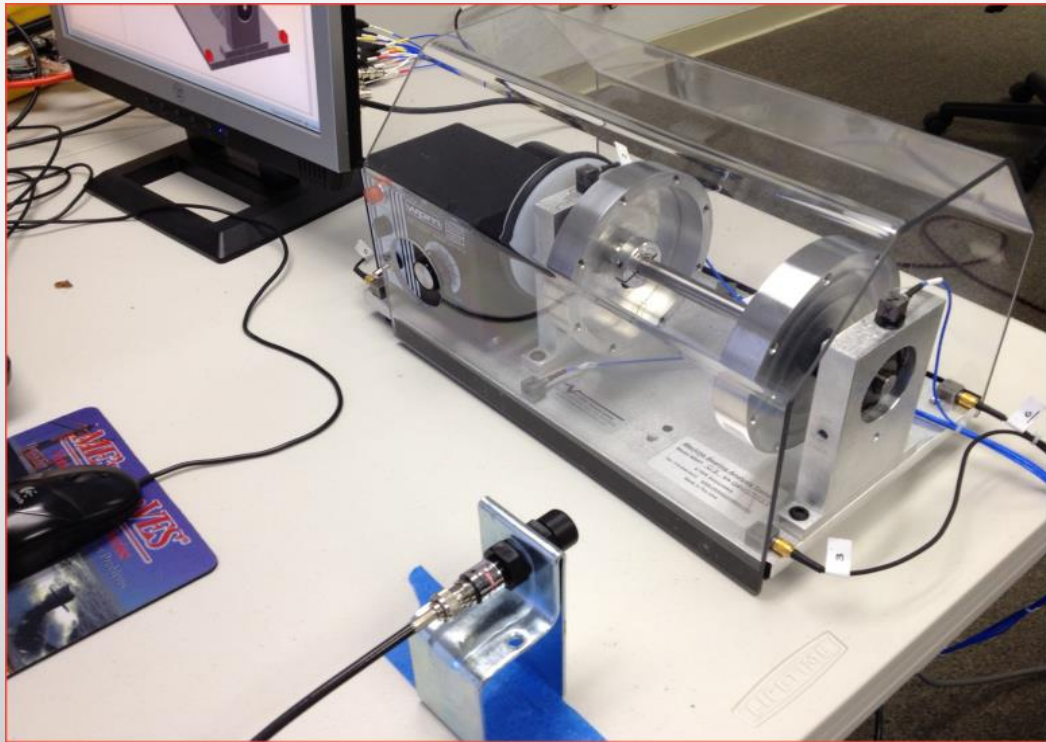
➤ **Two examples** will illustrate FLMA

1. **Order-based ODS's** of a rotating machine are **decomposed & expanded** from **24 DOFs** to **2000 DOFs**
2. **Sinusoidal response time waveforms** of a structure are **decomposed & expanded** from **99 DOFs** to **315 DOFs**

➤ In these examples only **FEA normal mode shapes** are used to **decompose & expand** experimental data

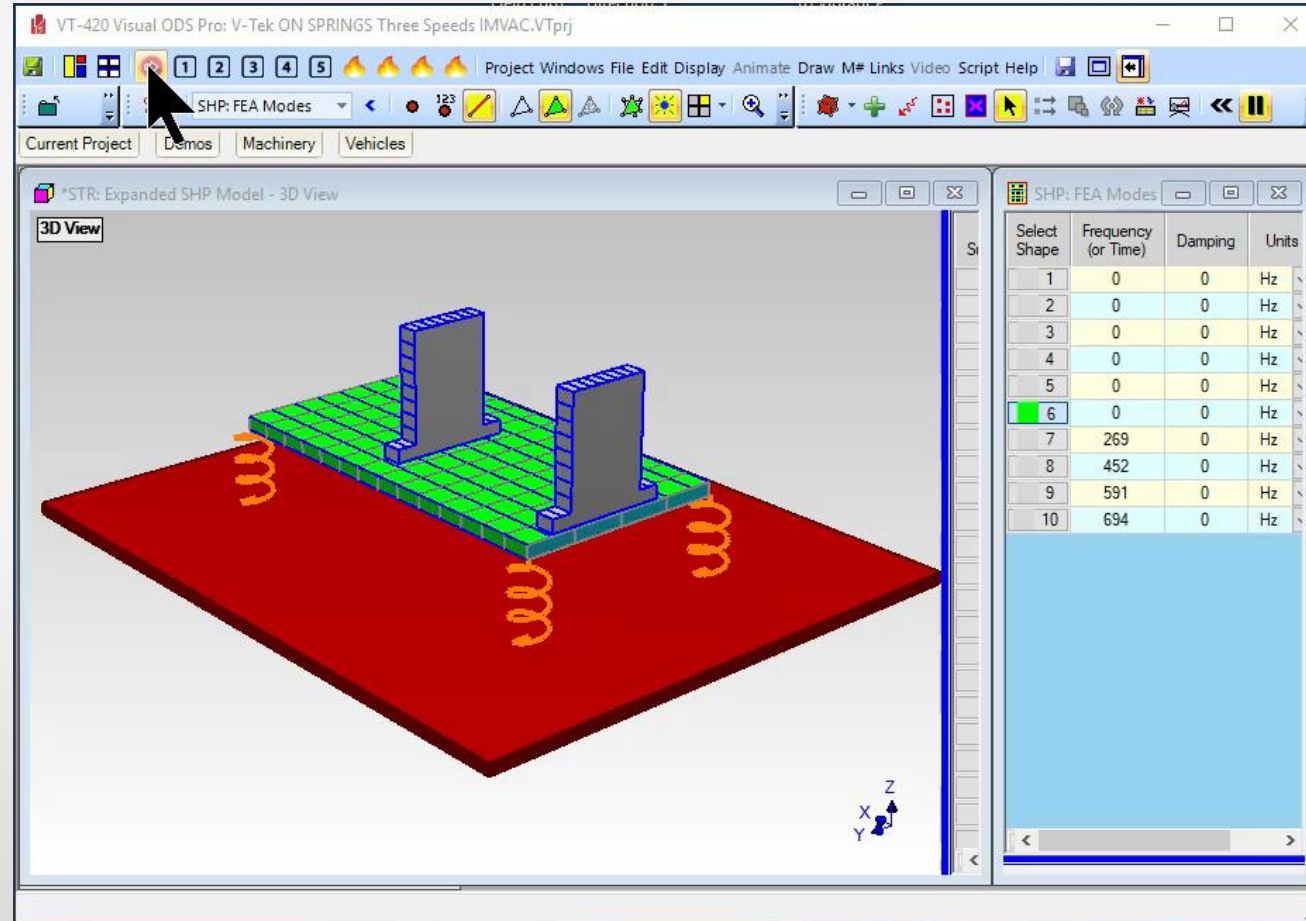
Example #1: Expanding a 24-DOF ODS

- Data was acquired from ***eight tri-axial accelerometers*** during operation of the rotating machine at ***985, 1440, & 2280 RPM***



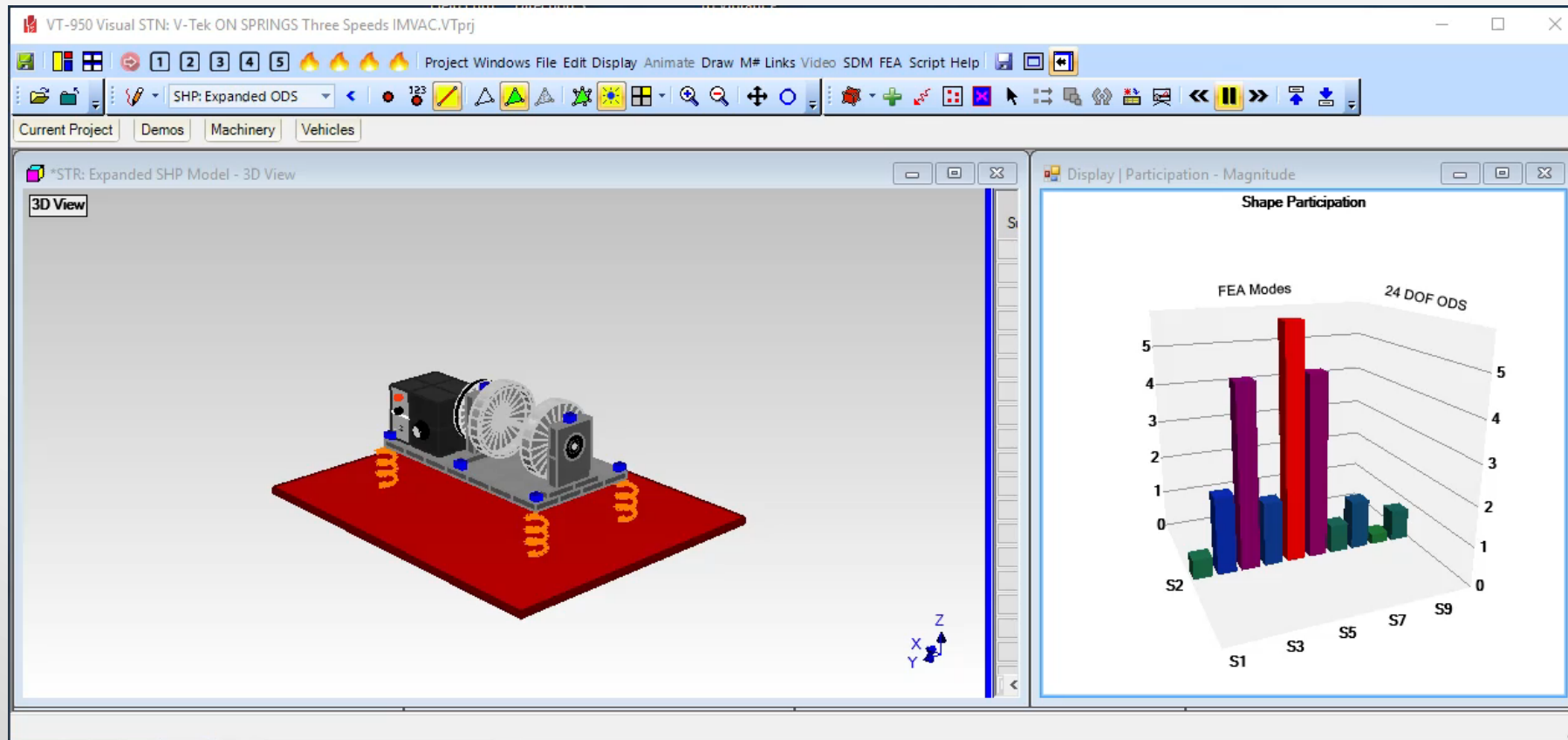
FEA Mode Shapes of the Base Plate & Bearing Blocks

- **Six Rigid Body** and **four Flexible Body** mode shapes were used to decompose & expand the ODS data



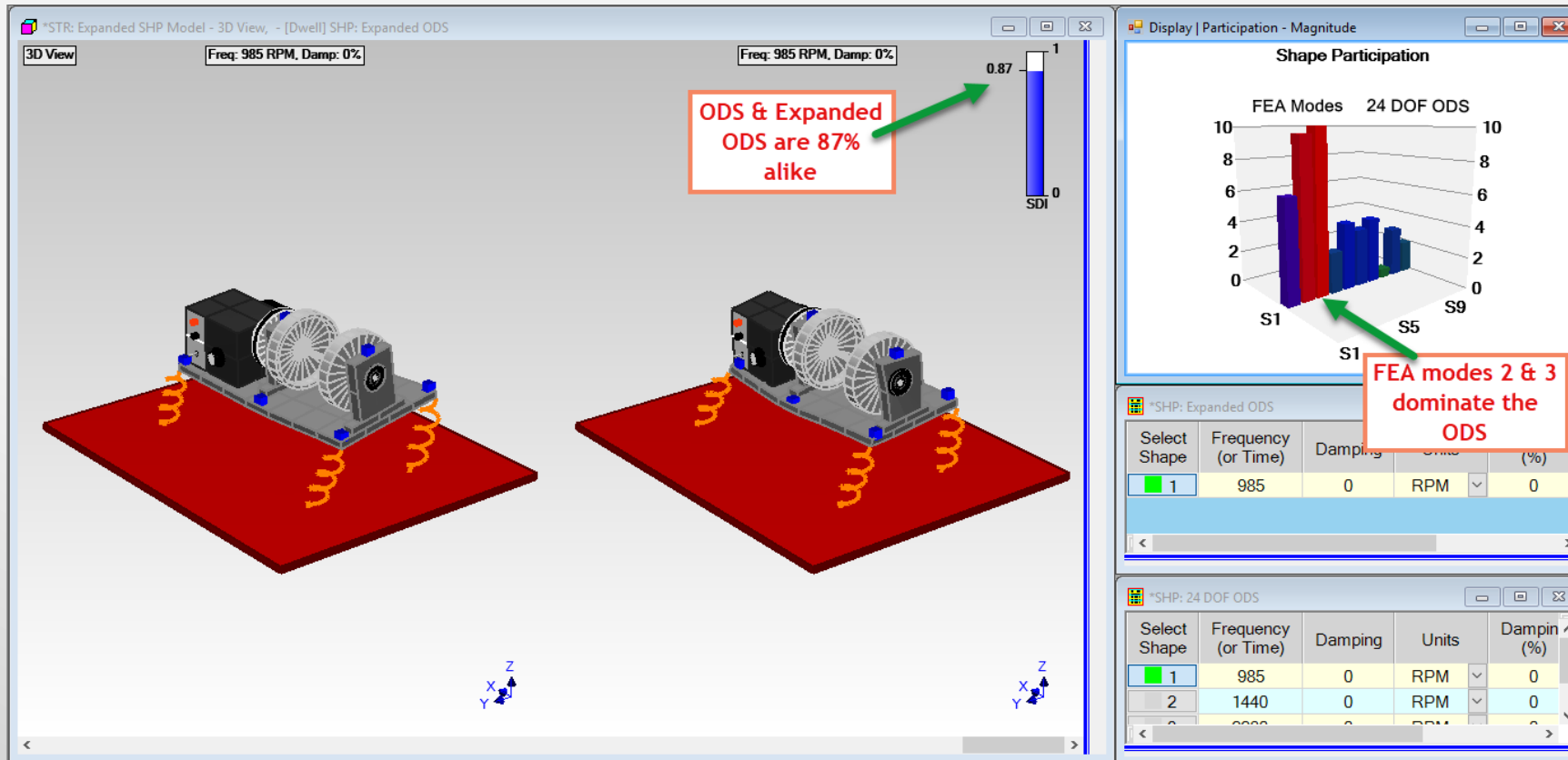
FEA Mode Shape Participation in the ODS at 985, 1440, & 2280 RPM

- Each ODS is **complex valued**. The FEA mode shapes are **normal (real valued) mode shapes**



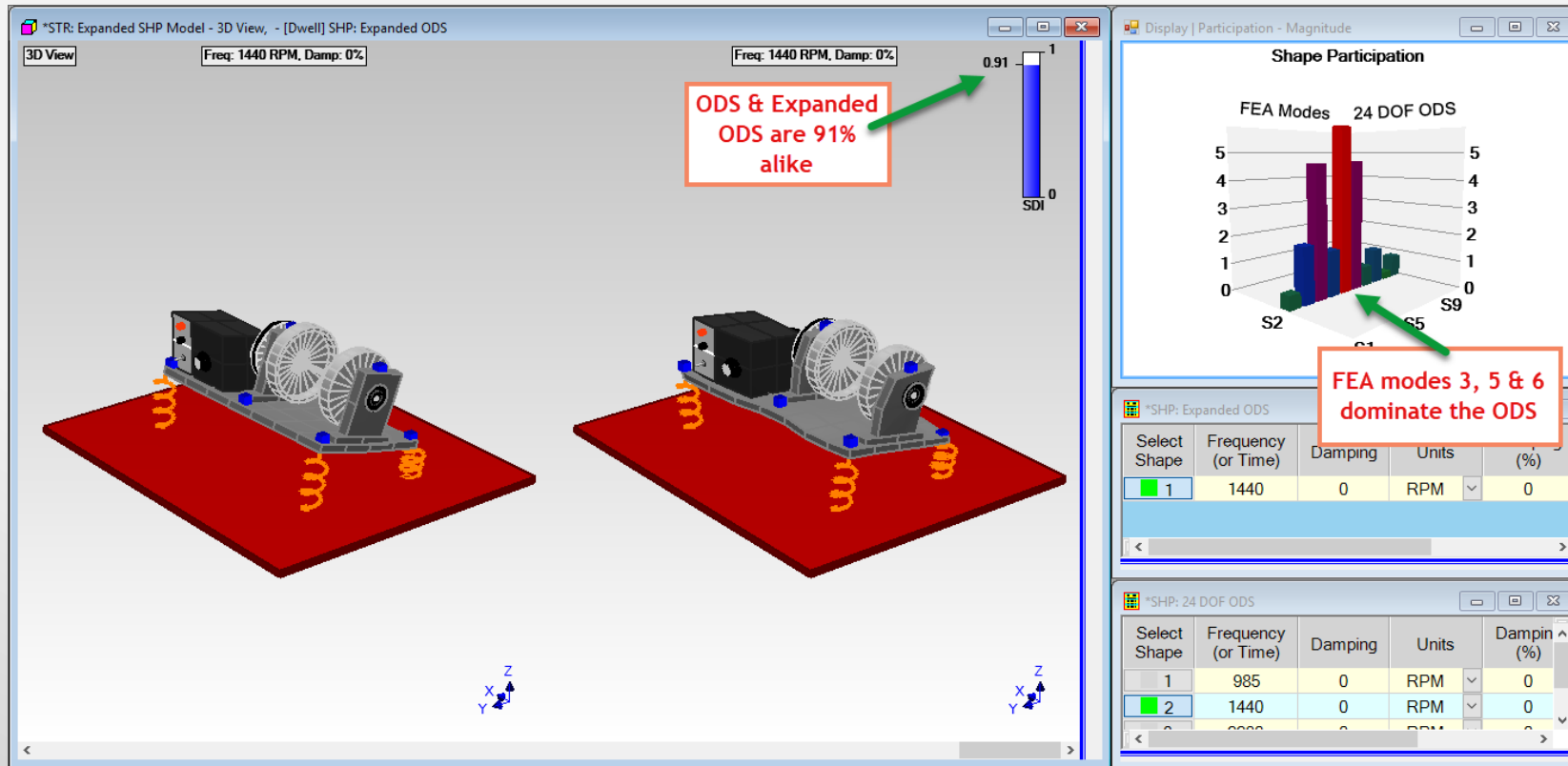
FEA Mode Shape Participation in the ODS at 985 RPM

- The **high SDI value** verifies that a **complex valued ODS** is accurately represented as a **summation of FEA normal mode shapes**



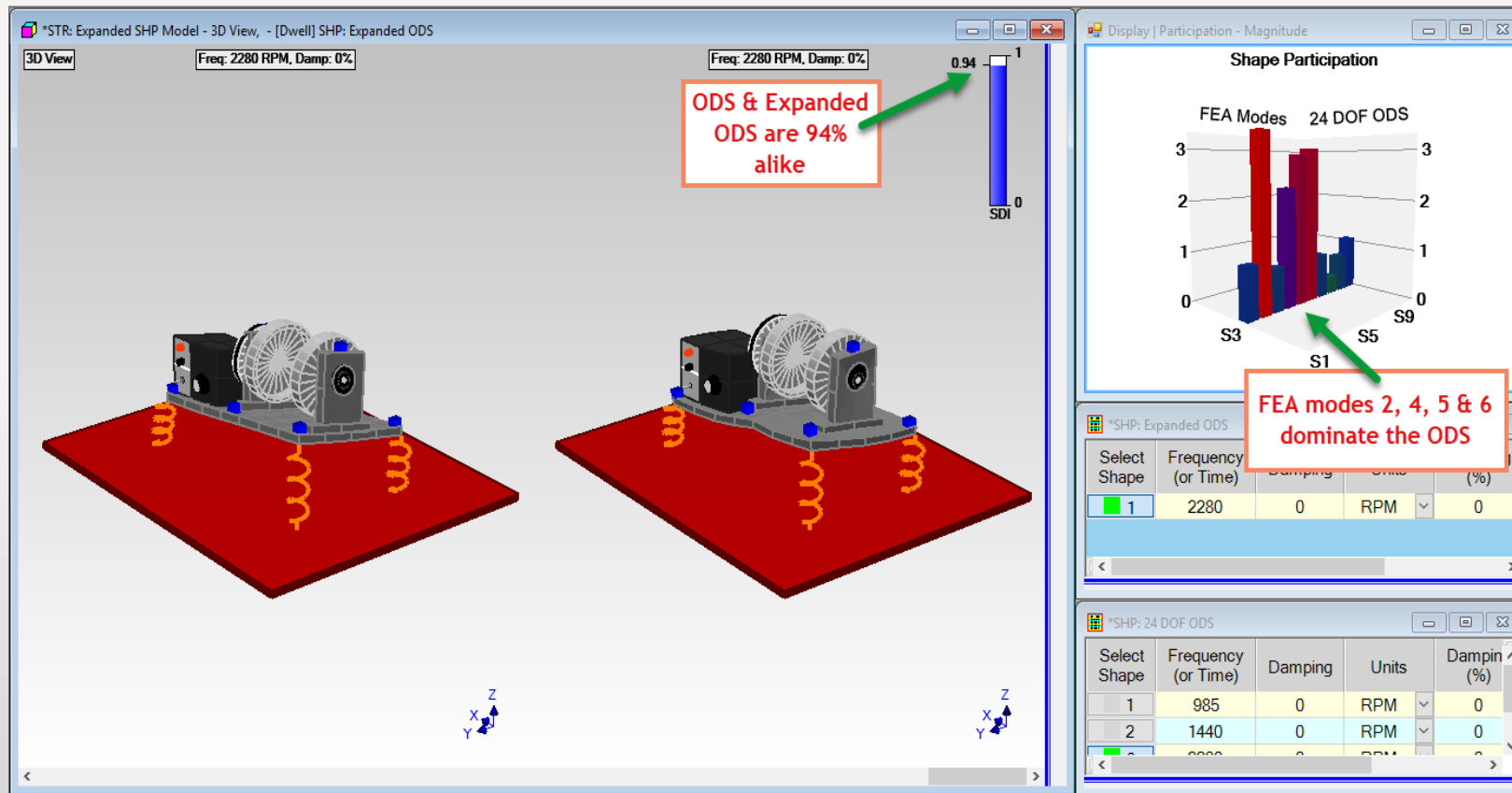
FEA Mode Shape Participation in the ODS at 1440 RPM

- The **high SDI value** verifies that a **complex valued ODS** is accurately represented as a **summation of FEA normal mode shapes**



FEA Mode Shape Participation in the ODS at 2280 RPM

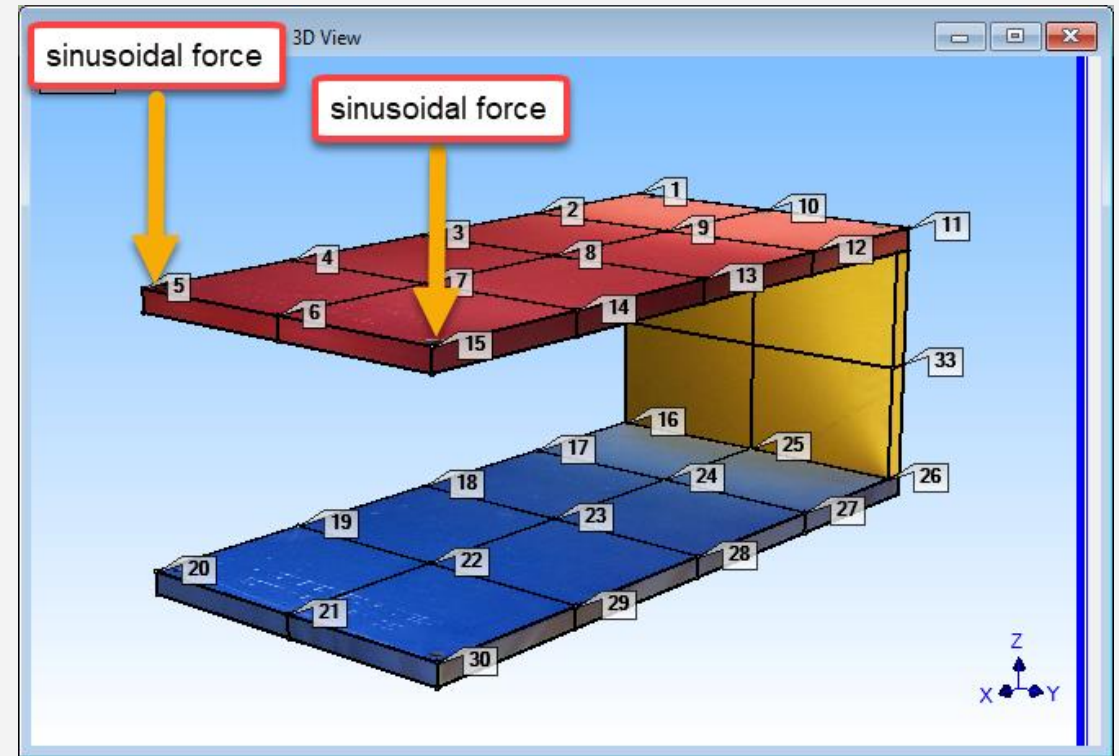
- The **high SDI value** verifies that a **complex valued ODS** is accurately represented as a **summation of FEA normal mode shapes**



Example #2: Expanding Sinusoidal Response Time Waveforms



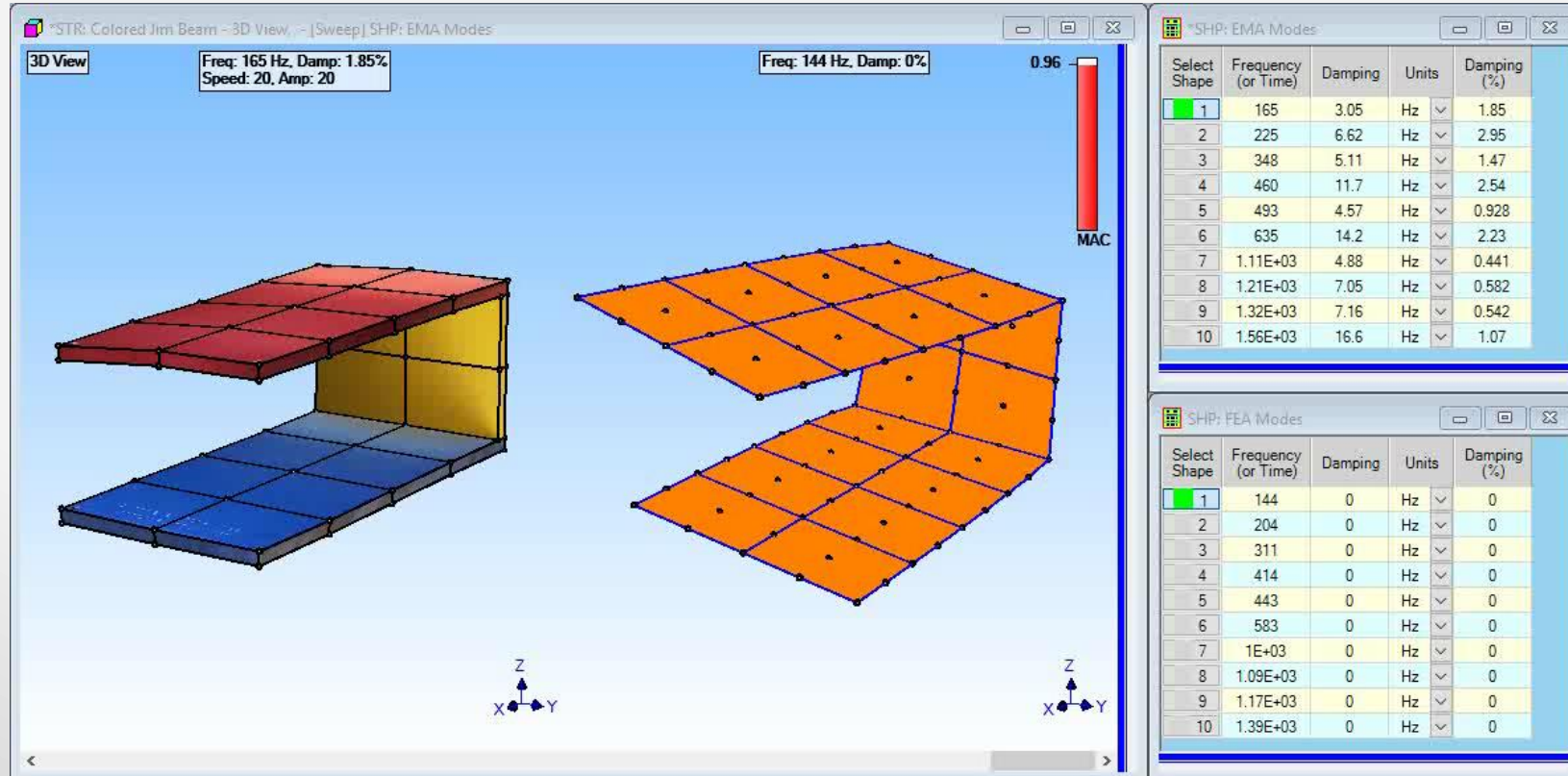
Impact Test using a Roving Tri-axial Accel



33 Test Points => Mode Shapes with 99 DOFs

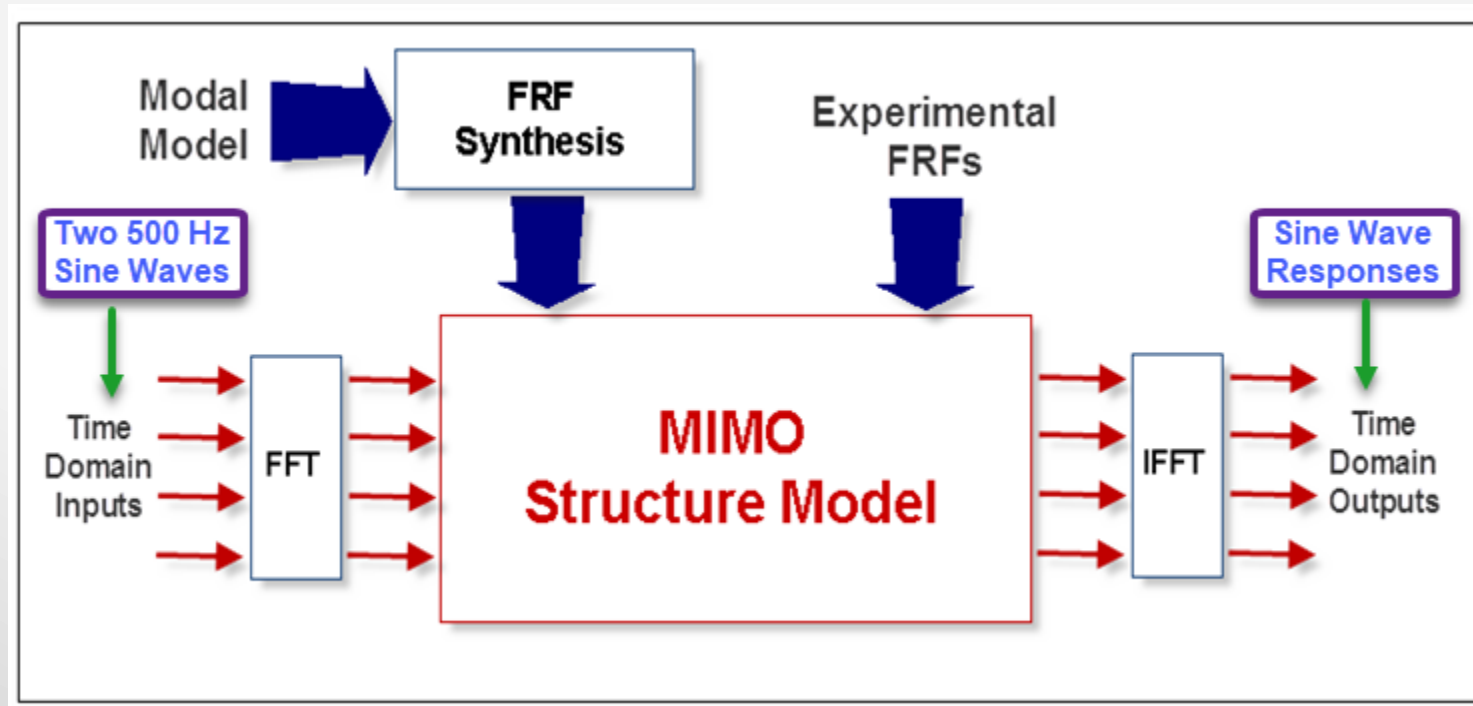
EMA & FEA Mode Shapes

- EMA mode shapes with **99 DOFs**, FEA mode shapes with **315 DOFs**
- **High MAC values** indicate **strong co-linearity** between EMA & FEA mode shapes



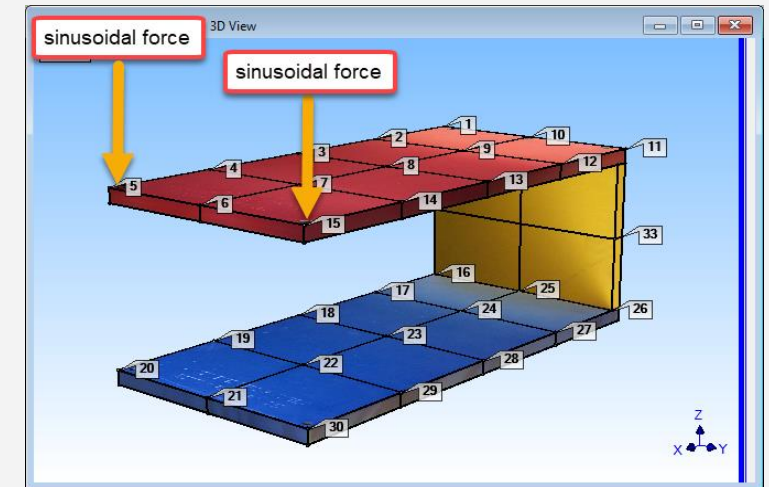
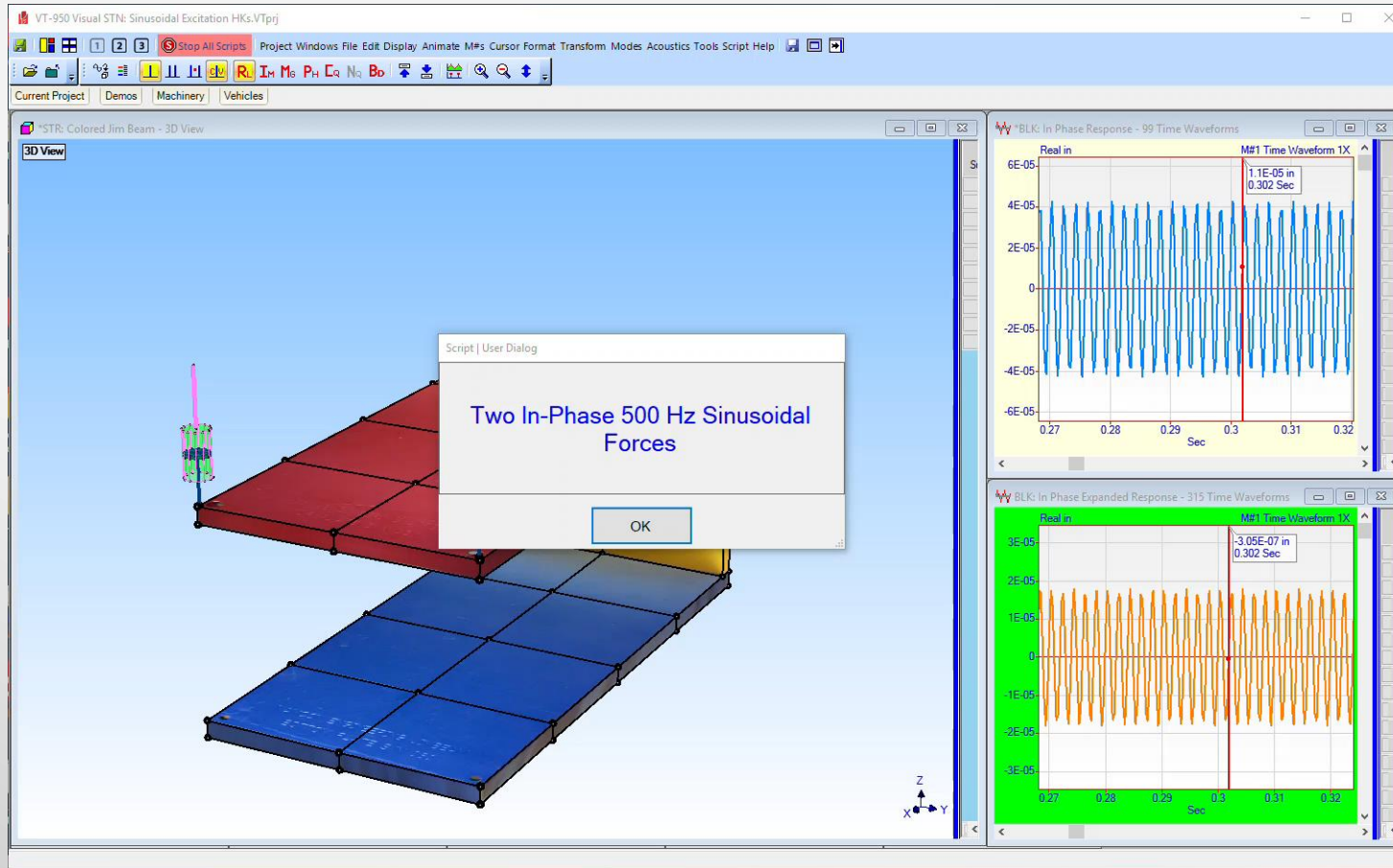
Two Sinusoidal Excitation Cases were Simulated

1. Two 500 Hz *In-Phase* sinusoidal excitation forces
2. Two 500 Hz *Out-of-Phase* sinusoidal excitation forces

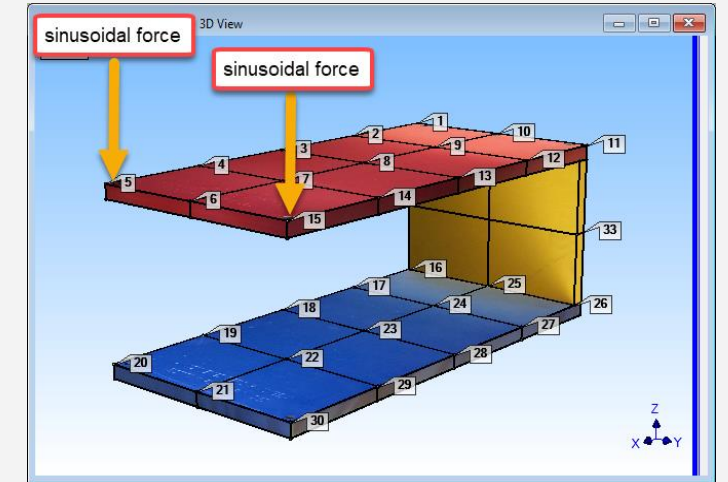
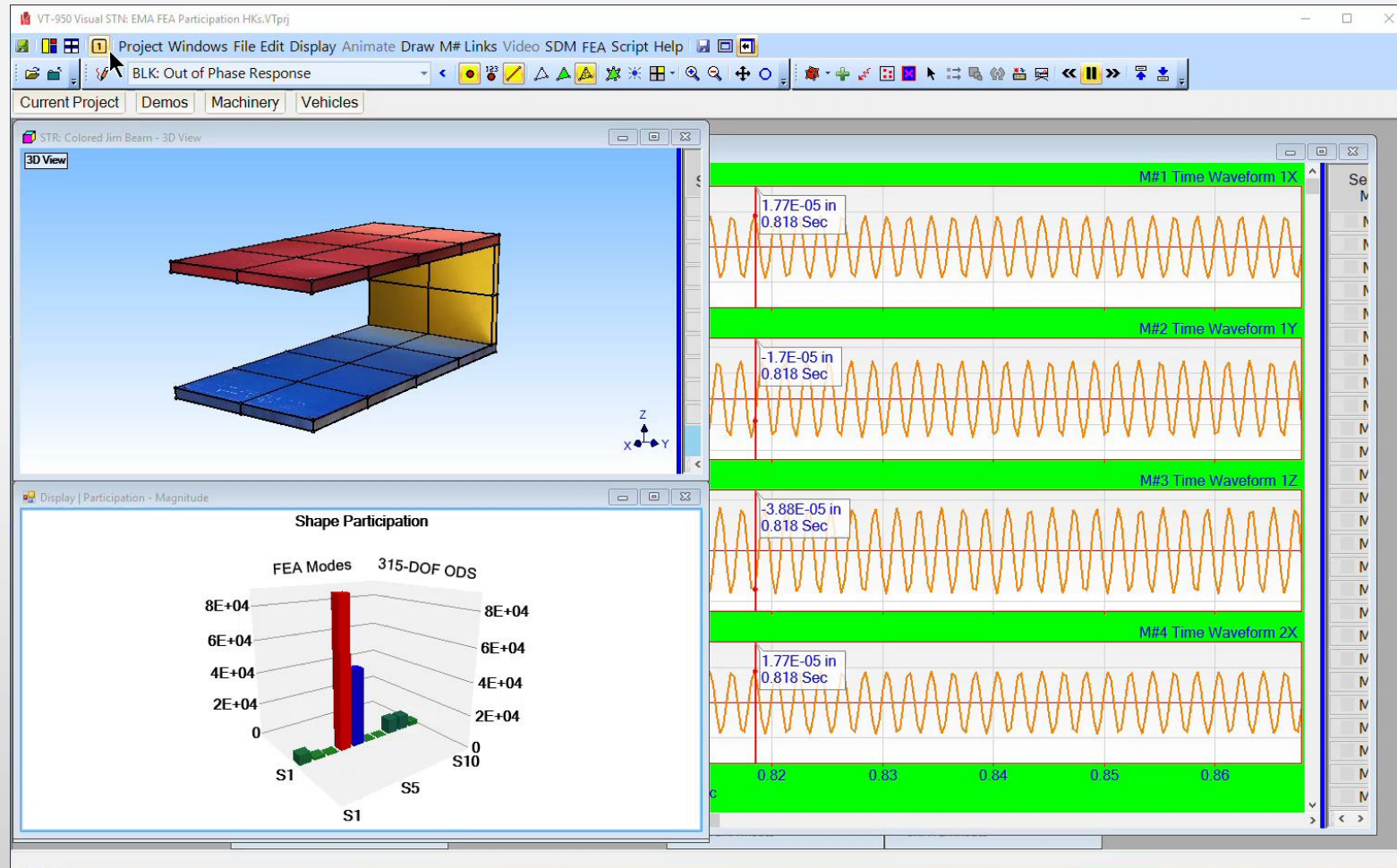


Responses to In-Phase & Out-of-Phase Excitation

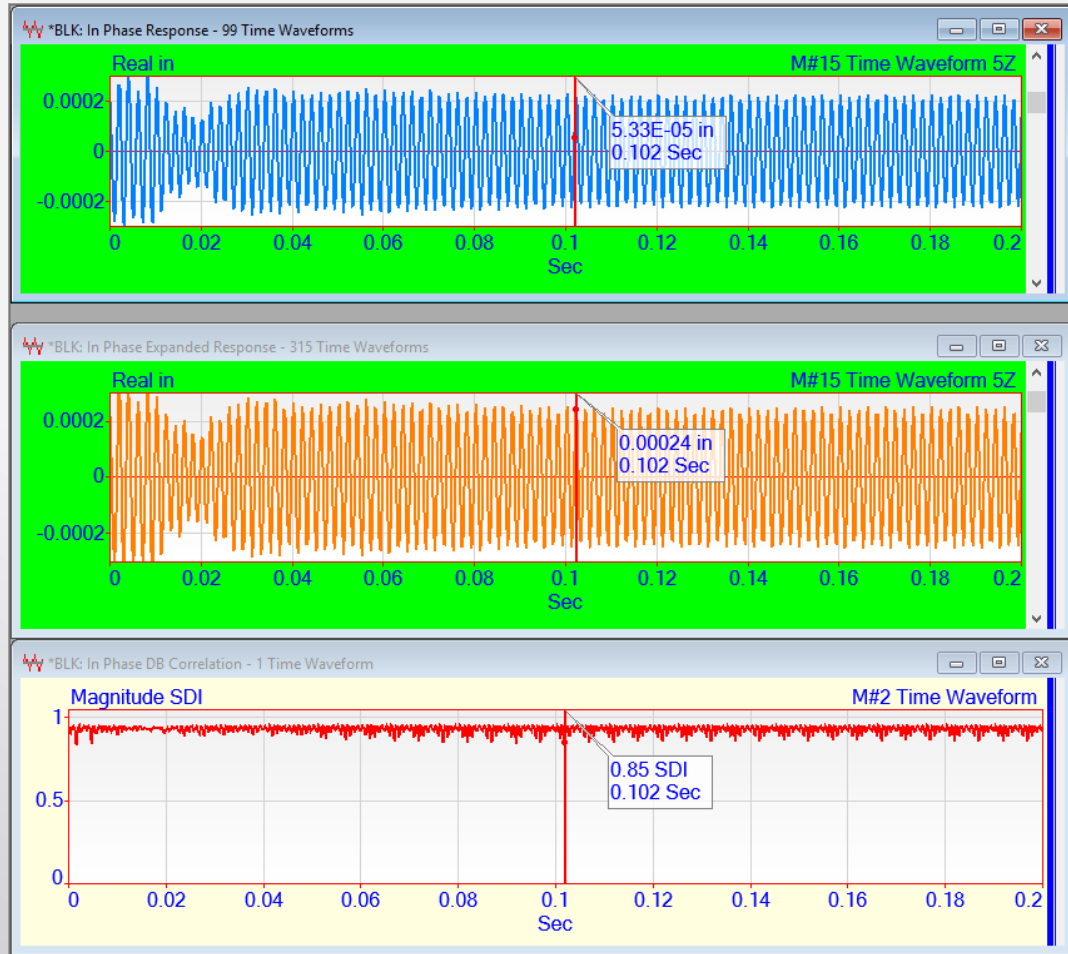
- **High MAC values** indicate **strong co-linearity** between EMA & FEA sinusoidal response



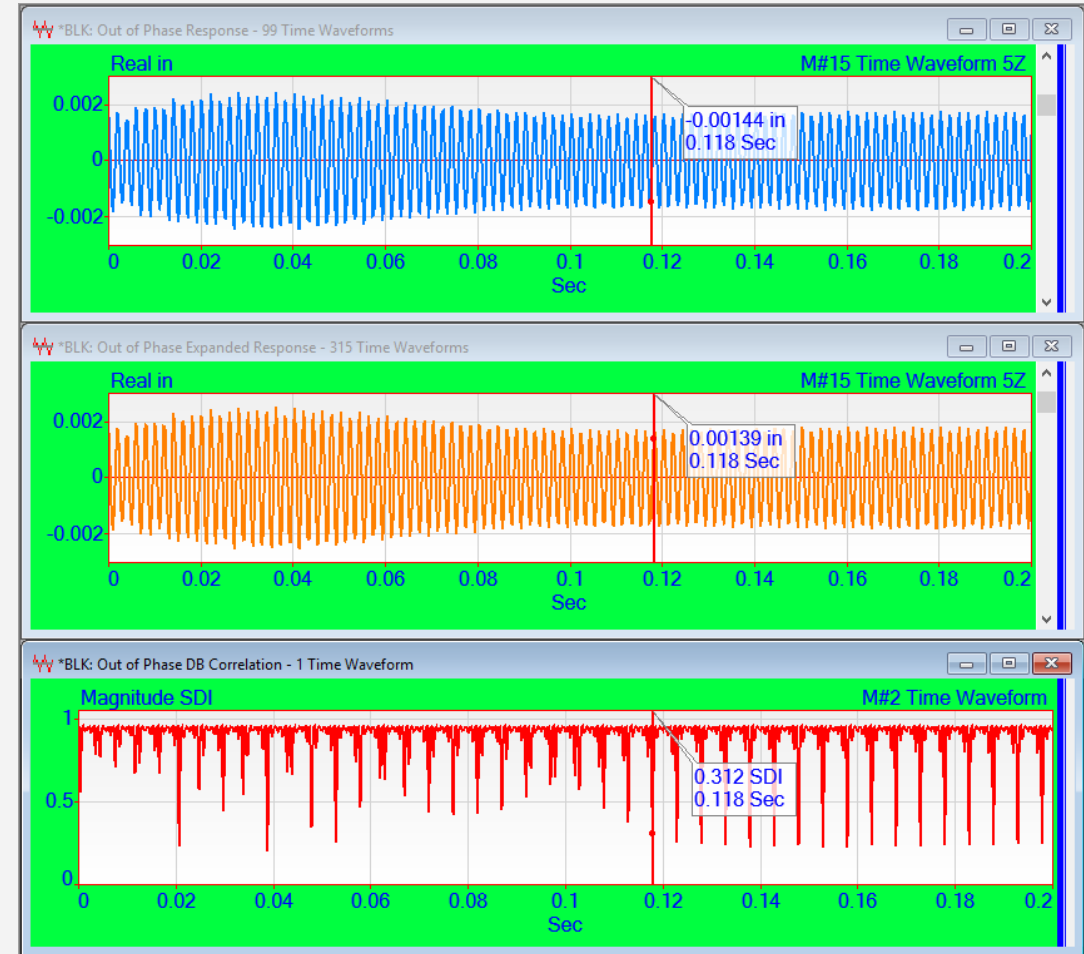
Mode Shape Participation - In-Phase & Out-of-Phase Excitation



Correlation Between EMA-Based & FEA-Expanded Responses



In-Phase Responses



Out-of-Phase Responses

Summary

- **Fundamental Law of Modal Analysis (FLMA)**: All vibration is a **summation of mode shapes**
- **FEA mode shapes** were used to **“decompose”** and then **“expand”** experimental data to include DOFs that were not experimentally acquired
- **Only FEA mode shapes** were used, not their frequency or damping
- Mode shapes from an **FEA model** with **free-free boundary conditions** and **no damping** were used
- **Complex** experimental data which includes **real-world boundary conditions** and **real-world damping** can be decomposed & expanded using **FEA normal mode shapes**